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HIGH PERFORMANCE POLYURETHANE ELASTOMERS. PART 2. MILLABLE ELASTOMERS AND SYNTACTIC FOAMS

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Explosives Research and Development Establishment Waltham Abbey, England

January 1972

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# EXPLOSIVES RESEARCH AND DEVELOPMENT ESTABLISHMENT

**TECHNICAL REPORT No. 83** 

High Performance Polyurethane Elastomers:
Part 2: Millable Elastomers and Syntactic Foams

B E Brokenbrow
D Sims
J Wright

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by

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# SUMMARY

Polyurethane elastomers based on millable sulphur cured polycaprolactone, polyoxy 1,4-butylene glycol and hydroxyl terminated polybutadiene/di-isocyanate precursors, chain extended with unsaturated diols, together with liquid cast polyoxy 1,4-butylene glycol di-isocyanate prepolymers filled with small hollow spheres (syntactic foams) were assessed to determine their resistance to water (80°C) and Standard Test Fluid (65°C). Two commercially supplied urethane elastomers, one based on a low molecular weight polyether/toluene di-isocyanate prepolymer cured with methylene-bis-(2-chloro-aniline), the other on a higher molecular weight polyether/4,4-methylene bis-cyclohexyl di-isocyanate prepolymer, cured with methylene bis-aniline were also assessed for comparison.

A millable caprolactone urethane elastomer gave fair resistance to STF at 65°C coupled with a very low permeability to STF at 30°C, whilst a millable polyether urethane elastomer gave good resistance to water at 80°C. A low density buoyant polyether based syntactic foam, filled either with hollow glass or 'fly-ash' spheres, gave good resistance to water at 80°C.

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Reference: WAC/213/025

#### 1 INTRODUCTION

## 1 1 Millable Elastomers

Previous reports by the present authors 1-6 have described the ageing properties of polyurethane elastomers prepared from liquid castings, during exposure These elastomers were prepared to various laboratory simulated environments. with hydroxyl terminated polyol/di-isocyanate prepolymers, cured with diols/ triols and/or diamines. However, other polyurethane elastomers 7,8 which are claimed to possess good resistance to oils and solvents and known as millable urethanes are cured either with sulphur or peroxides. advantages of millable urethane elastomers are that they are prepared with conventional rubber processing equipment and the curing systems used are likely to be less toxic than MOCA [methylene bis-(2-chloroanili.e)], which is widely used in high performance liquid casting urethane elastomers. addition, pigments and fillers such as carbor black may be more readily incorporated into the millable elastomers, thus possibly producing elastomers with superior physical properties and resistance to photo-oxidation compared with liquid cast polyurethane elastomers.

Uncured millable polyurethane elastomers are essentially thermoplastic materials capable of undergoing flow when processed on a rubber mill and contain reactive groups which may be crosslinked with suitable sulphur or peroxide curing agents. The polymer chain is usually linear or slightly branched, and unlike polyol/di-isocyanate prepolymers used for liquid castings which contain excess di-isocyanate; difunctional polyols and di-isocyanates are reacted in nearly stoichiometric proportions. Curing potential is introduced into millable urethane systems by the introduction of olefinic -C=C- groups, contained either in the relatively high molecular weight hydroxyl terminated polyol or in a relatively low molecular weight di- or tri-functional chain extender or crosslinking agent such as 2-butene 1,4-diol or trimethylol propane monoallyl ether.

With  $\epsilon$ -caprolactone based millable urethanes for example, unsaturation was achieved, either by the use of an unsaturated diol initiator and/or an unsaturated diol or triol chain extender.

Millable polyether based copolymers and terpolymers have been prepared using mixtures of cyclic oxides, such as tetrahydrofuran ethylene or propylene oxide and allyl glycidyl ether  $^{10}$  which yield  $-CH_2O - CH_2 - CH = CH$  as the R group pendant to the main chain.

Similarly, a millable polyurethane based on a commercially available polyether/toluene di-isocyanate prepolymer was used for comparative purposes in the present investigation, the polyol is polyoxy 1,4-butylene glycol in which unsaturation is introduced probably by the inclusion of 5 - 10 per cent glycerol alpha-allyl ether.<sup>11</sup>

The millable elastomers assessed in the present work were cured with sulphur, which involves the use of mixtures containing sulphur, catalysts and accelerators of the thiazole class, which are likely to form sulphur bridges

in the vicinity of unsaturated portions of the molecule, including monosulphide, polysulphide, vicinal polysulphide crosslinks and cyclic monosulphides. For comparative purposes a commercial low molecular weight polyoxy 1,4-butylene glycol/toluene di-isocyanate prepolymer cured with MOCA was also assessed.

# 12 Syntactic Foams

Polyurethane elastomers, which appear to bridge the gap between liquid castings and blown foams, may be prepared by dispersing hollow spherical fillers into liquid casting elastomers. A previous preliminary assessment of hydroxyl terminated polybutadiene urethane elastomers filled with hollow glass spheres 3 suggested that such materials may be of potential Service interest for applications where a hydrolytically stable buoyant low density Composites of this type prepared from elastomeric foam is required. polyester, epoxide, phenolic and polyvinyl chloride resins filled with small hollow glass and phenolic spheres 5 - 150 µm in diameter have been described previously. 12 These materials are commonly known as 'syntactic' foams (Greek 'syntaxis' meaning orderly arrangement). Suggested applications for such materials include deep submergence buoyancy, structural composites and load bearing insulation, rocket nose cones and fins, and sonor windows (some acoustic properties of syntactic foams are similar to seawater). 13,14 Similarly, hollow spheres of carbon filled with an inert gas have been used in nylon and epoxide resins and are of interest for application as low density heat shield for re-entry vehicles. 15 More recently it has been found that ash recovered from electricity generating stations which use pulverized coal as a fuel, contains a small proportion of low density thinwalled hollow spheres ('Cenospheres')16 of silicate glass 20 - 200 μm The use of 'Cenospheres' as a light-weight filler for electrical insulation, 17 in composite with cement, clay and resin binders 18 and as a buoyancy material 19 have been reported. 'Cenospheres' are said to be competitive in price with manufactured hollow-glass spheres. 18

In the present investigation the ageing properties of liquid cast elastomers based on a recently developed commercial polyether, believed to be polyoxy 1,4-butylene glycol (average mol wt 1900)/di-isocyanate prepolymer cross-linked with methylene bis-aniline, both unfilled and containing hollow spheres, were assessed. This particular polyether di-isocyanate prepolymer is of interest as the aliphatic di-isocyanate 4,4'-methylene bis-cyclohexyl di-isocyanate which is used is a material which we have not examined previously; also the curing agent methylene bis-aniline may be less toxic then methylene bis-(2-chloroaniline).

The main objectives of the present work were to prepare polyurethane millable elastomers and syntactic foams and to assess their ageing resistance in water at 80°C, STF, and diester lubricant, STF/water mixtures at 65°C.

# 2 MATERIALS AND METHODS OF PREPARATION

Brief details of the compositions of the elastomers are given below. Formulations and methods of preparation are described in the Appendix.

# 2 1 Millable Elastomers

			\$19 (g)		\$195 (g)		<b>1</b> 92 g)
poly ε-caprolactone/toluene di- trimethylol propane monoallyl		anate/	100		-		<b>-</b>
*polyoxy 1,4-butylene glycol/todi-isocyanate/glycerine alpha-eether			-		100	•	-
hydroxyl terminated polybutadic 4,4°-diphenyl methane di-isocya	ene/ anate		-		-	10	0
2-butere 1,4-diol			100		-	1	<b>3.</b> 6
carbon black HAF			<b>3</b> 0		<b>3</b> 0	3	0
2-benzothiazyl disulphide			4		4		4
mercaptobenzothiazole			1		1		1
sulphur			0	<b>-7</b> 5	0.75	,	0.75
zinc chloride/2-benzothiazyl d	iáe	0	• <i>3</i> 5	0.35	,	0.35	
cadmium stearate			0	•50	0.50		0.50
Polyether Control			S1 (g				
polyoxy 1,4-butylene glycol/to di-isocyanate prepolymer	luene		100				
methylene bis-(2-chloroaniline	.)		25				
*probable composition							
2 2 Syntactic Foams							
	\$211 (g)	\$2 <b>1</b> 2 (g)	S217 (g)	\$2 <b>1</b> 6 (g)	S218 (g)	\$2 <b>1</b> 9 (g)	
Polyoxy 1,4-butylene glycol/ 4,4*-methylene bis-cyclohexyl di-isocyanate/methylene bis-aniline elastomer	100	100	100	100	100	100	
Hollow glass spheres	-	12.5	18.0	20.0	-	-	-
Hollow carbon spheres	-	-	-	-	12.5	-	-
Hollow 'fly-ash' spheres	-	-	-	-	-	12.5	20.0

The reaction products were poured into PTFE coated steel trays and cured in an over for 16 h at 90°C to produce sheets 220 mm x 150 mm, 2.5 mm thick.

# 3 EXPERIMENTAL

# 3 1 Mechanical Properties

British Standard type C dumb-bell test pieces (five per test) were cut from the cast sheets and the width and thickness measured before exposure to the test conditions. Dumb-bells, in sets of five, were suspended in loosely stoppered glass tubes and exposed to some or all of the following environments:

Controls Conditioned in hir at 20°C

Hot/wet Immersed in boiled out distilled water at

80°C for 28 days

Phosphate Diester Lubricant Immersed in 'Skydrol' at 65°C for 9 days

\*Standard Test Fluid Immersed in STF at 65°C for 28 days

STF/Water 90/10 Immersed in STF/water mixture at 65°C for

10 days

The charged tubes were placed in circulating air ovens in which the temperatures did not vary by more than  $\pm$  0.5°C from the test temperature. After the required period of exposure the tubes and contents were removed from the oven and conditioned at room temperature for 24 hours before testing. After the conditioning period, the groups of five specimens were removed from the tubes, dried from superficial liquid, and tested for hardness, moduli, extension at break and tensile strength as quickly as possible. Hardness was measured using a micro-indentometer, and the tensile properties were measured by British Standard Methods 21,22 on a Hounsfield Type E Tensometer at a constant rate of extension of 500 mm/min. Unaged control specimens cut from the materials were tested by the same methods, and the results used as "unaged" reference points.

## 32 Permeability

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The permeability of selected elastomers to STF (petrol) at 30°C was determined by the method described. 23

#### 4 RESULTS AND DISCUSSION

The results of mechanical tests and the percentage changes in original properties of the urethane elastomers are summarised in Tables 1 and 3. The permeabilities of the elastomers to STF (petrol) at 30°C are compared with

<sup>\*</sup>Standard Test Fluid (STF) consists of a 70/30 v/v mixture of iso-octane and toluene, and is intended to represent a standard "medium to high aromatics" content petrol. 20

other typical synthetic elastomers in Table 2.

# 4 1 Millable Urethanes

Table 1 shows that both sulphur cured polyoxy 1,4-butylene glycol and polycaprolactone millable urethane elastomers gave satisfactory all round initial mechanical properties. In fact, sulphur cured polyether elastomers showed equally satisfactory initial properties to MOCA [methylene bis-(2-chloroaniline)] cured polyether urethanes previously examined. Although the sulphur cured hydroxyl terminated polybutadiene elastomer showed less satisfactory initial mechanical properties, the elastomer showed good resistance to water at 80°C, although its resistance to STF at 65°C was poor. The ageing properties of the elastomers were similar to those of diol and diamine cured hydroxyl terminated polybutadiene elastomers examined previously. The sulphur cured polycaprolactone urethane elastomer gave fairly good resistance to STF and STF/water mixtures at 65°C but poor resistance to water at 80°C. Table 2 below shows that the permeability of the millable polycaprolactone elastomer to STF at 30°C was low, and at least as good as the best of the synthetic elastomers which were evaluated for comparison. 23

On the other hand, the sulphur cured polyether elastomer whilst giving good resistance to water at 80°C was not resistant to STF and STF/water mixtures at 65°C. The MOCA cured low molecular weight polyether assessed for comparison, whilst giving good resistance to STF and STF/water mixture at 65°C showed poor resistance to water at 80°C.

None of the elastomers were capable of resisting phosphate based diester lubricant at 65°C.

TABLE 1

CHANGES IN MECHANICAL PROPERTIES OF MILLABLE POLYUPETHANE ELASTOMERS AFTER AGEING IN VARIOUS ENVI

		T							Percenta	ge
Code No	Elastomer type	ın:	itial prope (unaged)				28 days 80	in water		
		TS (MN/m²)	M 100 (MN/m²)	EB (%)	H (BS°)	TS	M 100	EΒ	н	
<b>\$1</b> 92	hydroxyl terminated polybutadiene/ sulphur cure	7•5	•••	75	93	<b>-15.</b> 0	-	- 7.0	- 1.0	-
<b>S194</b>	polycaprolactone/ sulphur cure	29.2	5•3	345	84	Too weak to test				-
S195	polyether/sulphur cure	26.1	4.2	380	78	-11.0	-48.0	+ 36.0	-18.0	-
<b>S1</b> 96	polyether/MOCA cure (control)	35.1	33.0	115	99	-47.0	<b>-61.</b> 0	<b>+150.</b> 0	-10.0	-

Key: TS = tensile strength at break

M 100 = modulus at 100 per cent extension EB = percentage extension at break H = hardn MOCA = methy

TABLE 2

Code No	Elastomer
S192	sulphur cured hydroxyl terminated polybutadiene urethane
<b>\$1</b> 94	sulphur cured polycaprolactone ureth
S195	sulphur cured polyether urethane
<b>\$19</b> 6	MOCA cured polyether urethane
	Nitrile
	PVC/nítrile
	Neoprene WRT

# RTIES OF MILLABLE POLYURETHANE ELASTOMERS AFTER AGEING IN VARIOUS ENVIRONMENTS

T	tial man						Percenta	ge change	of ori	ginal me	chanical	propert
111.	itial prope (unaged)	)			28 days 80	in water			28 day 65	ys STF C		
TS (MN/m²)	M 100 (MN/m²)	EB (%)	H (BS°)	TS	<u>м</u> 100	EB	Н	TS	M 100	EB	Н	us
<b>7.</b> 5	**	75	93	<b>-15.</b> 0	••	- 7.0	- 1.0	-60.0	-	-20.0	<b>-</b> 35•0	<b>-71.</b> 0
29•2	5•3	345	84		Too weak to test				<b>-25.</b> 0	-20.0	-19.0	<b>-</b> 56 <b>.</b> 0
26.1	4.2	380	78	-11.0	-48.0	+ 36.0	<b>-1</b> 8.0	<b>-</b> 59 <b>.</b> 0	<b>-</b> 55 <b>.</b> 0	-20.0	<b>-36.</b> 0	-57.0
35•1	33.0	<b>11</b> 5	99	-47.0	<b>-61.</b> 0	<b>+1</b> 50.0	-10.0	-21.0	0.0	<b>-1</b> 9.0	0.0	-42.0

rength at break 100 per cent extension extension at break H = hardness

MOCA = methylene bis-(2-chloroaniline)

TABLE 2

Code No	Elastomer	Thickness (mm)	Permeability (ml/m²/day)
<b>S1</b> 92	sulphur cured hydroxyl terminated polybutadiene urethane	2 <b>.1</b> 5	3640
S194	sulphur cured polycaprolactone urethane	1.68	57
S <b>1</b> 95	sulphur cured polyether urethane	1.83	530
<b>\$1</b> 96	MOCA cured polyether urethane	1.34	<b>1</b> 570
	Nitrile	2.0	220
	PVC/nitrile	2.0	<b>1</b> 45
	Neoprene WRT	2.0	1 <b>1</b> 60

ING IN ARIOUS ENVIRONMENTS

-													
	Percenta	ge change	e of ori	ginal me	chanical	property	y after a	ageing fo	or				
water		28 days STF 9 day 65°C						FF/Water 10 65°C		10	days 600	Skydro C	01
<b>E</b> B	Н	TS	M 100	EB	Н	TS	<u>M</u> 100	EΒ	н	TS	TS M EB I		
7.0	- 1.0	<b>-50.</b> 0	-	<b>20.</b> 0	<b>-35.</b> 0	<b>-</b> 71 <b>.</b> 0	•	<b>-</b> 33•0	<b>-</b> 42 <b>.</b> 0		Too we to ter		
reak est		-40.0	-25.0	-20.0	-19.0	<b>-</b> 56 <b>.</b> 0	-47.0	- 6.0	-37.0	Too weak to test			
<b>36.</b> 0	<b>-1</b> 8.0	<b>-</b> 59 <b>.</b> 0	<b>~</b> 55.0	-20.0	<b>-36.</b> 0	-57.0	+ 1.0	+ 1.0	<b>-51.</b> 0	Too weak to test			
<b>150.</b> 0	-10.0	-21.0	0.0	<b>-1</b> 9.0	0.0	-42.0	-47.0	+39.0	0.0		Too we		

H = hardness

MOCA = methylere bis-(2-chloroaniline)

<u> </u>		
stomer	Thickness (mm)	Permeability (ml/m²/day)
roxyl terminated thane	2.15	3640
caprolacton a hane	1.68	57
ether urethane	1.83	530
er urethane	1.34	<b>1</b> 5 <b>7</b> 0
	2.0	220
	2.0	145
	2.0	<b>11</b> 60

TABLE : CHANGES IN MECHANICAL PROPERTIES OF MILLABLE POLYURETHANE ELASTOMERS AFTER AGEING IN VARIOUS ENVIRONMENTS

		• 1							Percentage change of original mechanical property, after ageing for	e change	of orig	nal mec	nanical	property	after o	seing for				
Elastomer type	4 95	Š	Initial properties (unaged)	rties	·		8 days 80	28 days in water			28 days STF 65°C	STF		6	9 days STF/Water 90/10 65°C	Water 65°C		10 d.	10 days Skydrol 60°C	drol
:		TS (HN/m²)	100 (MN/m²)	<b>∄</b> ⊛	H (BS°)	TS	¥ 02	83	н	TS	₩ 100	В	æ	ŢS	×δ	A	m	TS	× &	# #
hydroxyl terminated polybutadiene/ sulphur cure	ene/	7.5	ı	75	93	-15.0	ı	- 7.0	- 1°C	0.09-	t	0.02-	-35.0	-71.0	,	-33.0	-45.0	4 13	Too weak to test	
polycaprolactone/ sulphur cure	lactone/ ure	29.5	5.3	345	7.8		Too	Too weak to test		0.04-	-25.0	-20.0	-19.0	-56.0	0-44-	0.9 -	-37.0	E4 43	Too weak to test	
polyether	polyether/sulphur cure	26.1	7.5	&	78	-11.0	-48.0	0.0% + 0.84-	-18.0	-59.0	-55.0	-20.0	-36.0	-57.0	-57.0 + 1.0 + 1.0	1.0	-51.0	EH P	Too weak to test	
polyether/MOCA cure (control)	r/MOCA	35.1	33.C	115	8	-42.0	ó-19 <del>-</del>	-61.9 +150.0	-10.0	-21.0	0.0	-19.0	0.0	-45.0	0.74-	+39.c	0.0	₩ ₩	Too wrak to test	

Key: TS = tensile strength at break
H 100 = modulus at 100 per cent extension
EB = percentage extension at break

H c hardness MOCA s methylene bis-(2-chloroaniline)

TABLE 2

Code	Elastomer	Thickness (mm)	Permeability (ml/m²/day)
5192	sulphur cured hydroxyl terminated polybutadiene urethane	2.15	3640
5194	sulphur cured polycaprolactone urethane	1.68	25
\$195	sulphur cured polyether urethane	1.83	530
3196	MOCA cured polyether urethane	1.34	1570
	Nitrile	2.0	220
	PVC/nitrile	2.0	145
	Net rene WRT	2.0	1160

k 3

TABLE 3

CHANGES IN HECHANICAL PROPERTIES OF SYNTACTIC POLYURETHANE FOAMS AFTER AGELMG IN VARIOUS ENVIRONMENTS

		я		-35.0	-34.0	-32.0	-37.0	•	•
	FF/Water	<b>a</b>	3	0.0	-16.0	+25.0	+18.0	+14.0	-21.0
Percentage change of original mechanical property after ageing for	9 days STF/Water	×δ	,	-76.0	-75.0	+ 5.0	-89.0	-62.0	-61.0
after a		£ St	63	-65.0	-67.0	-37.0	-53.0	-62.0	-60.0
property		×	13.0	-17.0	J.85-	-39.0	-18.0		
hanical	STF 65°C	g	45.0	-50.0	-12.0	-33.0	-23.0	0.34-	-48.0
nal mec	28 days STF 65°C	×β	54.0	-95.0	-85.0	-78.0		-33.0	-31.5
of orig		Ts	-58.0	-61.0	-55.0	-72.0	-54.0	-60.0	0.44-
e change	٥	<b>H</b>	-20.0	- 9.5	1.0	-16.5	429.0	•	
ercentag	28 days water 80°C	83	+35.0		+18.5	+29.5	+36.0	+17.0	0.87+
4	8 days w	×δ	-45.0	-43.5	-35.0	-59.5	-90.0	-24.1	-29.6
		ST.	- 2.5	0	+15.0	438.0	-53.0	- 5.1	+55.0
_		н (ВЗ <sup>о</sup> )	93	8	8	8	, 86	76	95
oroperties	(F	(%) (%)	8	8	215	230	195	325	9 <del>,</del> 2
Initial pro	` a	Н 100 (МN/m <sup>2</sup> )	8.9	7.8	4.0	5.9	4.8	5.8	5.4
Ini		TS (MN/m²)	24.8	12.1	5.4	7.6	6.3	11.9	7.3
	Additive (% by wt)	}	lın	glfss spheres (12.5)	glass spheres (18.0)	glass upheres (20)	caroon spheres (12.5)	'fly-ash' spheres (12.5)	'fly-ash' spheres (20.0)
•	Elastoner				Polyether/	4,4'-methylene bis-cyclohexyl	methylene bis-anline	•	
-	ş ç		5210	\$211	\$212	\$217	\$216	\$218	\$219

Key: TS = tensile strength at break M 100 = modulus at 100 per cent extension

EB = percentage extension at break
H = hardness

4.5

TABLE 3

CHANGES IN MECHANICAL PROPERTIES OF SYNTACTIC POLYURETHANE FOAMS AFTER AGEING IN VARIOUS ENV

			Tn	itial prop	erties			P	er
Code No	Elastomer	Additive (% by wt)	<b>3-11</b>	(unaged	2	8 days w	iat 		
NO	type	(so by we)	TS (MN/m²)	M 100 (MN/m²)	EB (%)	H (BS <sup>o</sup> )	TS	M 100	
\$210		nil	24.8	8.9	270	93	- 2.5	-45.0	T
S211	Polyether/ 4,4'-methylene bis-cyclohexyl di-isocyanate/ methylene bis-aniline	glass spheres (12.5)	12.1	7.8	200	97	0	-43.5	
\$21 <i>?</i> \$21 <i>7</i>		glass spheres (18.0)	5.4	4.0	2 <b>1</b> 5	90	+15.0	-35.0	
		glass spheres (20)	7.6	5•9	270	90	+38.0	<b>-</b> 59•5	
\$2 <b>1</b> 6		carbon spheres (12.5)	6.8	4,8	<b>1</b> 95	98	<b>-</b> 53 <b>.</b> 0	-90.0	T
\$218		'fly-ash' spheres (12.5)	<b>11.</b> 9	5.8	325	94	- 5.1	-24.1	T
<b>S21</b> 9		'fly-ash' spheres (20.0)	7.3	5.4	240	95	+55.0	-29.6	T

Key: TS = tensile strength at break

M 100 = modulus at 100 per cent extension

7.1

EB = perce H = hardn

7.7-

# OF SYNTACTIC POLYURETHANE FOAMS AFTER AGEING IN VARIOUS ENVIRONMENTS

	Tn	itial prop	enties			P	ercentage	e.change	of orig	inal mec	nanical p	roperty
<b>tiv</b> e	111.	(unaged			28	28 days water 80°C 28 days STF 65°C						
wt)	TS (MN/m²)	M 100 (MN/m²)	EB (%)	H (BS <sup>o</sup> )	TS	M 100	EB	Н	TS	и 100	<b>E</b> B	Н
2	24.8	8.9	270	93	93 - 2.5 -45.0 +35.0 -20.0 -58.0 -54.0					<b>-15.</b> 0	-17.0	
<b>(12.</b> 5)	12.1	7.8	200	97	0	-43.5	+35,0	<b>-</b> 9•5	-61.0	<b>-</b> 95 <b>.</b> 0	<b>-</b> 50 <b>.</b> 0	-17.0
(18.0)	5.4	4.0	215	90	+15.0 -35.0 +18.5 - 1.0 -55.0					-85.0	-12.0	<b>-</b> 58 <b>.</b> 0
(20)	7.6	5•9	270	90	+38.0	<del>-</del> 59•5	+29•5	<b>-1</b> 6 <b>.</b> 5	<b>-72.</b> 0	<b>-</b> 78.0	-33.0 -39.0	
(12.5)	6.8	4.8	195	98	<b>-</b> 53 <b>.</b> 0	-53.0 -90.0 +36.0 +29.0 -54.0						-18.0
(12.5)	11.9	5.8	325	94	- 5.1	-24.1	+17.0	-	-60.0	-33.0	<b>-</b> 48.0	-
(12.5) (22.0)	7.3	5.4	240	95	+55.0	-29.6	+50.0	us	-44.0	~31.5	-48.0	-

at break
r cent extension
7.

EB = percentage extension at break
H = haldness

7.3

7.2

ING IN VARIOUS ENVIRONMENTS

	Pe	ercentage	e.change	of origi	inal mecl	nanical p	property	after a	geing for	r	
28	days wa	ater 80°		6	28 days 1	stf 65°c		9 days STF/Water 90/10 65°C			
TS	<b>M</b> 100	EB	Ħ	TS	M 100	<b>E</b> B	Н	TS	M 100	EB	Н
- 2.5	<del>-</del> 45 <b>.</b> 0	+35•0	-20.0	<b>-</b> 58 <b>.</b> 0	54.0	<b>-1</b> 5.0	-17.0	<b>-</b> 62 <b>.</b> 0	<b>-</b> 56 <b>.</b> 0	-19.0	<b>-27.</b> 0
0	-43.5	+35•0	<b>-</b> 9•5	-61.0	<del>-</del> 95 <b>.</b> 0	<b>-</b> 50 <b>.</b> 0	-17.0	-65.0	-76.0	0.0	<b>-</b> 35•0
+15.0	-35.0	+18•5	- 1.0	<del>-</del> 55 <b>.</b> 0	<b>-</b> 85 <b>.</b> 0	-12.0	<b>-</b> 58 <b>.</b> 0	-67.0	<b>-7</b> 5 <b>.</b> 0	-16.0	-36.0
+38.0	<del>-</del> 59•5	+29•5	<b>-1</b> 6 <b>.</b> 5	<b>-7</b> 2 <b>.</b> 0	<b>-</b> 78.0	<del>-</del> 33 <b>.</b> 0	-39.0	-37.0	+ 5.0	+26.0	-37.0
<b>-</b> 53 <b>.</b> 0	<b>-</b> 90 <b>.</b> 0	+36.0	+29•0	-54.0	1	-23.0	-18.0	<b>-</b> 53 <b>.</b> 0	-89.0	+18.0	-37.0
- 5.1	-24.1	+17.0	•	<b>-</b> 60 <b>.</b> 0	<b>-</b> 33 <b>.</b> 0	-48.0	_	-62.0	<b>-</b> 62 <b>.</b> 0	+14.0	
+55.0	<b>-</b> 29 <b>.</b> 6	+50.0	-	-44.0	<del>-</del> 31.5	<b>-</b> 48.0	-	-60.0	-61.0	-21.0	-

EB = percentage extension at break
H = hardness

73

# 4 2 Syntactic Foams

The addition of hollow spheres to a liquid cast polyether urethane elastomer based on a polyoxy 1,4-butylene glycol/4,4: methylene bis-cyclohexyl di-isocyanate propolymer cured with methylene bis-aniline produced buoyant composites of lower density, tensile strength and 100 per cent modulus compared with the unfilled elastomer. Optimum processing characteristics were obtained with 121 to 20 per cent 'fly-ash' and glass spheres, whilst additions of more than 121 per cent carbon spheres produced elastomers with Similarly, optimum mechanical poor flow and casting characteristics. properties both initially and after ageing were obtained with additions of hollow spheres at loadings of  $12\frac{1}{2}$  per cent rather than 20 per cent. the initial mechanical properties of the glass and 'fly-ash' filled elastomers were somewhat inferior to the unfilled elastomers they showed satisfactory resistance to water at  $80^{\circ}\text{C}_{\circ}$ . Elastomers filled with carbon spheres gave inferior resistance to water compared with glass and 'fly-ash' filled materials, but their resistance to STF/water mixture at 65°C was rather better than either unfilled 'fly-ash' or glass filled elastomers. The unfilled MOCA free polyether urethane elastomer showed good resistance to water although its resistance to STF and STF/water mixtures at 65°C was poor.

## 5 CONCLUSIONS

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A range of methylene bis-(2-chloroaniline) (MOCA) free urethane elastomers based on sulphur cured millable elastomers and liquid cast elastomers filled with hollow spheres (syntactic foam) were prepared and evaluated.

Sulphur cured, carbon black filled polycaprolactone and polyether urethane elastomers gave good mechanical properties initially. The polycaprolactone elastomer was very impermeable to STF at 30°C and showed fairly good retention of physical properties after 28 days' immersion in STF and STF/water at 65°C; the resistance of the elastomer to water at 80°C however, was poor. The polyether elastomer on the other hand, showed good resistance to water at 80°C but poor resistance to STF and STF/water at 65°C and was inferior in this respect to a MOCA cured liquid cast polyether urethane evaluated for comparison. None of the elastomers was found to be capable of resisting phosphate diester lubricant at 65°C.

Buoyant, low density syntactic foams prepared from a polyether urethane filled with hollow spheres showed fairly good mechanical properties coupled with good resistance to water at 80°C, although the resistance of these materials to STF, as well as the unfilled polyether evaluated for comparison, was poor. The unfilled polyether based on a polyoxy 1,4-methylene glycol/4,4'-methylene bis-cyclohexyl di-isocyanate cured with methylene bis-aniline, which is probably less toxic than MOCA, gave good mechanical properties initially, coupled with very good resistance to water at 80°C.

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APPLINDIX

# FORMULATIONS AND METHODS OF PREPARATION

## MILLABLE ELASTOMERS

Formulations of gum stocks

S194

		mole equivalent
a	NIAX 520 polycaprolactone polyol (av mol wt 830, hydroxyl no 135, acid no 0.3)	0•5
	NIAX 540 polycaprolactone polyol (av mol wt 1250, hydroxyl no 90, acid no 0.3)	0•5
b	Hylene TM, a mixture of 80: 202,4 and 2,6 isomers toluene di-isocyanate	2.0
С	trimethylol propane monoallyl ether	1.0

## Method

THE STREET STREE

The mixed caprolactone polyols and the trimethylol propane were heated to 65°C under nitrogen in a three-necked Quickfit 500 ml flask equipped with stirrer, thermometer and nitrogen inlet and stirred until homogeneous. The toluene di-isocyanate was added and the mixture stirred for 30 minutes at 80 - 85°C. The reaction product was poured into PTFE coated aluminium trays and cured for 12 h at 100°C.

\$195 was a commercially supplied polyether urethane known as

d Adiprene CM and is probably based on the following formulation

		mole equivalent
	polyoxy 1,4-butylene glycol	1.0
	toluene di-isocyanate	2.0
С	glycerine alpha-monoallyl ether	1.0
S192		
		mole equivalent
e	Hydroxyl terminated polybutadiene R.15M (OH functionality 2.3)	1.0
f	Isonate 143L (modified 4,4'-diphenyl methane di-isocyanate)	2.3

## APPENDIX

## Method

The hydroxyl-terminated polybutadiene was heated to 105°C in a three-necked 'Quickfit' flask equipped with stirrer, thermometer, nitrogen and vacuum inlet, the resin was degassed for 30 minutes under 5 mmHg, vacuum cooled to 40°C and Isonate 143L added. Stirring was continued to 1 h at 40 - 50°C and the prepolymer degassed for 5 minutes under 1 mmHg vacuum. The reaction product was poured into PTFE coated aluminium trays and cured for 16 h at 95 - 100°C.

# Formulations of Elastomers

	S195	unded st S195 by weig	<b>S1</b> 92
Gum stock S194 caprolactone/TDI prepolymer	100	-	-
" S195 polyoxy 1,4-butylene glycol/TDI prepolymer	-	100	-
" " S192 hydroxyl terminated polybucadiene/MDI prepolymer	•	-	100
2-butene 1,4-diol	-	-	13.6
g carbon black HAF	30	30	30
2-benzthiazyl disulphide	4	4	4
mercaptobenzothiazole	1	1	1
sulphur	0.75	0 <b>.7</b> 5	0.75
h zinc chloride/2-benzthiazyl disulphide	0.35	0.35	0.35
cadmium stearate	0.50	0.50	0.50

The above mixes were dispersed on a 'Bridge' Rubber mill and press cured for  $\frac{1}{2}$  in at  $120^{\circ}$ C.

S196 Liquid Cast Polyether Urethane

		g
i	Polyoxy 1,4-butylene glycol (av mol wt 500)/toluene di-isocyanate prepolymer (9.5% free NCO)	250
	Methylene-bis-(2-chloroaniline) 86% theoretical	62.5

# Key to Suppliers

- a Niax 520 and Niax 540, Caprolactone polyols ex-Union Carbide.
- b Hylene TM, toluene di-isocyanate ex Du-Pont (UK).
- c Trimethylol propane monoallyl ether and glycerine alpha-allyl ether ex-Kodak.
- d Adiprene CM, millable polyether urethane ex-Du Pont (UK).
- e R.15M, hydroxyl terminated polybutadiene ex-Arco Chemicals.
- f Isonate 143L, modified 4,4°-diphenyl methane di-isocyanate ex-Upjohn.
- g Carbon black HAF ex-Cabot Chemicals.
- h Caytur 4 ex-Du Pont.
- i Polyether prepolymer ex-Du Pont.

Syr	Syntactic foams	\$240 (Unfilled elastomer for comparison)	S211 (pan	1 S212 S217 (parts by weight)	S217 eight)	<b>S</b> 216	S218	S219
.D	Polyoxy 1,4-butylene ¿iycol (av mol wt 1900) 4,4'-methylene bis-cyclohexyl di-isocyanate prepolymer (4.75%) free NCO) 100 parts cured with methylene bis- aniline (95% theory) 10.6 parts	\$ \$	8	8	6	100	100	100
×	Hollow glass spheres	ı	12.5	18.0	20.0	ı	ı	ı
н	Hollow carbon spheres	ı	ı	ŀ	ı	12.5	i	•
8	Hollow 'fly-ash' spheres	ı	ı	ı	ŧ		12.5	20.0
Met	Method of preparation (unfilled elastomer S210)	mer S210)						
The ani	The polyether prepolymer was heated to 105°C and degassed under 1 mmHg vacuum for 5 minutes, methylone bis- aniline preheated to 110°C was added to the prepolymer with stirring, the mixture was degassed for 3 minutes at 105°C and the reaction product poured into PTFE coated aluminium trays and cured for 16 h at 100°C.	105°C and degassed under o the prepolymer with sti ed into PTFE coated alumi	r 1 mmHg irring, † inium tra	vacuum the mixt ays and	for 5 mit ure was d cured for	nutes, me legassed . 16 h at	for 3 mi	bis- nutes

Was V.

Method of preparation (syntactic foams)

The method of preparation was the same as described above, except that the spheres were added to the polyether prepolymer, dispersed by stirring and the mixture degassed for 10 minutes at  $90 - 100^{\circ}$ G, prior to the addition of MDA curing agent.

# APPENDIX

# Key to Suppliers

- j Polyether prepolymer Adiprene LD 2699 ex-Du Pont (UK).
- k Armospheres ex-JBC Plastics (Dewsbury).
- 1 Carbo-Spheres ex-General Technologies Corp US.
- m Cenospheres ex-Central Electricity Research Laboratories, Leatherhead.

Technical Report No 83

Explosives Research and Development Establishment

HIGH TEAFORMANCE POLYMETHANE ELASTOFERS: PART 2: MILLABLE ELASTOFERS AND
SINTACTIC FOAMS

Brokenbrow B E, Sims D, Wright J
January 1972
15 pp. 3 tabs, nc figs

Folywrethane elastomers based on millable sulphur cured polycaprolactone, polycay 1,4-butylene glycol and hydroxyl terminated polybutadiene/diIsocyanate precursors, chain extended with unsaturated diols, together with liquid chat polyoxy 1,4-butylene glycol di-isocyanate prepolymers filled with mail hollow spheres (syntactic foams) were assessed to determine their resistance to water (80°C) and Standard fest Fluid (65°C). Two commercially resistance to water some standard fest Fluid (65°C). Two commercially toluene di-isocyanate prepolymer cured with methylene-bis-(2-chloroanlline), the other on a higher molecular weight polyether/4,4,4-methylene bis-cyclo-hexyl di-isocyanate prepolymer, cured with methylene bis-aniline were also assessed for comparison.

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FOR FORMANCE B. Sims D. Wright J

January 1972 15 pp, 3 tabs, no figs Polyurethane elastomers based on millable sulphur cured polycaprolactone, polyoxy 1,4-butylene glycol and hydroxyl terminated polybutadiene/di-Isocyanate precursors, chain extended with unsaturated diols, together with liquid cast polyoxy 1,4-butylene glycol di-Isocyanate prepolymers filled with small hollow spheres (syntactic foams) were assessed to determine their resistance to water (80°C) and Standard Test Fluid (65°C). Two commercially supplied urethane elastomers, one based on a low molecular weight polyether/toluene di-Isocyanate prepolymer cured with methylene-bis-(2-chioroaniline), the other on a higher molecular weight polyether/ty,tf\*-methylene bis-cyclonhexyl di-Isocyanate prepolymer, cured with methylene bis-aniline were also assessed for compatison.

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A millable caprolactone urethane clastomer gave fair resistance to STF at 65°C coupled with a very low permeability to STF at 30°C, whilst a millable 65°C opolyether urethane clastomer gave good resistance to water at 80°C. A low density buoyant polyether based syntactic foam, fillet either with hollow densit glass or fily-ash spheres, gave good resistance to water at 60°C.

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